



# Practical Design of Digital Filters Using the Pascal Matrix

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## Abstract

*In the context of the design of digital filters many research has been done to facilitate their computation. The Pascal matrix recently defined in (Biolkova and Bolek, 1999) has proved its utility in this field. In this paper we summarize the direct transform from the lowpass continuous-time transfer function  $H(s)$  to the discrete-time  $H(z)$  of the following main types of digital filters: lowpass, highpass and bandpass. An alternative representation of the original bandpass Pascal matrix is developed in this paper that permits to convert systematically the lowpass continuous-time prototype to the discrete-time bandpass transfer function. We also consider the inverse transformation from the discrete-time domain to the continuous one and we show that the inverse transformation is easily obtained as the determinant of the system need not to be computed. Several numerical examples illustrate the practical utilization of this technique.*

**Keywords:** Filter design, s-z transformation, Pascal matrix, digital filter design tools.

## Resumen

En el contexto del diseño de filtros digitales se ha desarrollado mucha investigación para facilitar su cálculo. La matriz de Pascal definida recientemente (Biolkova and Bolek, 1999) ha probado su utilidad en este campo. En este artículo se hace una síntesis de la transformación directa a partir de la función de transferencia pasa-bajas en tiempo continuo  $H(s)$  para obtener la de tiempo discreto  $H(z)$  de cada uno de los tres tipos principales de filtros digitales: pasa-bajas, pasa-altas y pasa-banda. También se desarrolla una representación alternativa de la matriz de Pascal pasa-banda original, que permite la conversión sistemática de un prototipo pasa-bajas en tiempo continuo a la función de transferencia pasa-banda en tiempo discreto. Adicionalmente se considera la transformación inversa a partir del dominio de tiempo discreto, al de tiempo continuo y se demuestra que esta transformación inversa es fácil de calcular, dado que no es necesario obtener el determinante del sistema. Varios ejemplos numéricos ilustran la utilización práctica de esta técnica.

**Descriptores:** Diseño de filtros, transformaciones s-z, matriz de Pascal, herramientas para el diseño de filtros digitales.

## Introduction

A large number of procedures are available for designing digital filters (Parks and Burrus, 1987); (Antoniou, 1993). Many of them transform a given analog filter into an equivalent digital filter. The digital filter design process begins with the synthesis or specification of the filter transfer function. A signal  $x(t)$  presented to a filter characterized by its impulse response  $h(t)$  produces an output  $y(t)$  given by the convolution  $y(t)=x(t)*h(t)$  or, if using the continuous-time transforms of the signals, by  $Y(s)=X(s)H(s)$ . Then the continuous-time circuit of a filter is completely described by the transfer function:

$$H(s) = \frac{A_0 + A_1s + A_2s^2 + \dots + A_ms^m}{B_0 + B_1s + B_2s^2 + \dots + B_ms^m} \quad (1)$$

From this equation the vectors  $\bar{A}$  and  $\bar{B}$  representing respectively the coefficients of the numerator and denominator can be defined as:

$$\begin{aligned} \bar{A} &= (A_0, A_1, A_2, \dots, A_m) \\ \bar{B} &= (B_0, B_1, B_2, \dots, B_m) \end{aligned} \quad (2)$$

where,  $A_i$  and  $B_i$  are real coefficients.

In the discrete-time domain the  $z$  transforms of the signals are used, and a digital filter is characterized by the transfer function:

$$H(z) = \frac{a_0 + a_1z^{-1} + a_2z^{-2} + \dots + a_nz^{-n}}{b_0 + b_1z^{-1} + b_2z^{-2} + \dots + b_nz^{-n}} \quad (3)$$

With real coefficients  $a_i$  and  $b_j$ .

The problem of the systematic conversion from the continuous-time prototype transfer function  $H(s)$  to its discrete-time version  $H(z)$

is addressed in this paper considering three types of conversions: *lowpass-to-lowpass*, *lowpass-to-highpass* and *lowpass-to-bandpass*. The original Pascal matrix (Biolkova and Biolek, 1999) is used to achieve this systematization, and an alternative representation of the original Pascal matrix is developed in this paper to rich the *lowpass-to-bandpass* conversion.

The remainder of this paper is organized as follows. Section II describes the *lowpass-to-lowpass* conversion. Section III adapts the previous development to the *lowpass-to-highpass* case. Section IV main contribution of this paper, develops an alternative representation of the original bandpass Pascal matrix which allows the *lowpass-to-bandpass* conversion. Section V presents the inverse conversion from the discrete-time domain to the continuous-time. In Section VI we give examples to illustrate all the cases.

## Lowpass-to-lowpass Transformation

For lowpass filters the digital transfer function  $H(z)$  can be obtained from the continuous-time prototype (1) using the bilinear  $s$ - $z$  transformation (Parks and Burrus, 1987):

$$s = c \frac{z-1}{z+1} \quad (4)$$

where

$$c = \cot \frac{\pi f_1}{f_s} \quad (5)$$

and the constants  $f_1$  and  $f_s$  represent the lowpass corner and sampling frequencies, respectively.

From the transfer function (3), we define the vectors  $\bar{a}$  and  $\bar{b}$  whose elements are respectively the coefficients of the numerator and denominator (Klein, 1976):

$$\begin{aligned} \bar{a} &= (a_0, a_1, a_2, \dots, a_n) \\ \bar{b} &= (b_0, b_1, b_2, \dots, b_n) \end{aligned} \tag{6}$$

In order to express the numerator vectors  $\bar{a}$  in terms of  $\bar{A}$  and denominator vectors  $\bar{b}$  in terms of  $\bar{B}$ , we replace the variable  $z$  in (1) by (4) then comparing the numerators and the denominators of the resulting transfer functions in  $z$  we can identify the coefficients by equating the coefficients of the like powers in  $z$ .

Thus, for  $n=2$  and  $m=2$  we obtain the following expression:

$$\begin{aligned} H(z) &= \frac{a_0 + a_1 z^{-1} + a_2 z^{-2}}{b_0 + b_1 z^{-1} + b_2 z^{-2}} = \\ &= \frac{A_0 + A_1 c + A_2 c^2 + z^{-1} (2A_0 - 2A_2 c^2) +}{B_0 + B_1 c + B_2 c^2 + z^{-1} (2B_0 - 2B_2 c^2) +} \tag{7} \\ &\quad \frac{+z^{-2} (A_0 - A_1 c + A_2 c^2)}{+z^{-2} (B_0 - B_1 c + B_2 c^2)} \end{aligned}$$

From the numerators the coefficients,  $a_i, i=0,1,2$  are easily identified and re-written in acquire the following matrix equation

$$\begin{bmatrix} a_0 \\ a_1 \\ a_2 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ 2 & 0 & -2 \\ 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} A_0 \\ A_1 c \\ A_2 c^2 \end{bmatrix} \tag{8}$$

In a similar manner, a matrix equation can be obtained for the coefficients,  $b_i, i=0,1,2$  of the denominator vector  $\bar{b}$ .

Using a more compact representation both equations can be written as follows:

$$\begin{aligned} \bar{a} &= \bar{P}_{LP}^{(n)} \times \bar{A} \\ \bar{b} &= \bar{P}_{LP}^{(n)} \times \bar{B} \end{aligned} \tag{9}$$

where  $\bar{P}_{LP}^{(n)}$  is the *lowpass* Pascal matrix defined in (Pòeni,,ka et al., 2002) and the vectors  $\bar{A}, \bar{B}$  are represented by

$$\begin{aligned} \bar{A} &= (A_0, A_1 c, A_2 c^2, \dots, A_m c^m) \\ \bar{B} &= (B_0, B_1 c, B_2 c^2, \dots, B_m c^m) \end{aligned} \tag{10}$$

As demonstrated in (Pòeni,,ka et al., 2002) the computation of the  $\bar{P}_{LP}^{(n)}$  matrix can be done in a systematic form. For this we consider the classical Pascal Triangle

|   |   |    |    |   |   |     |
|---|---|----|----|---|---|-----|
|   |   |    |    |   | 1 | n=0 |
|   |   |    |    | 1 | 1 | n=1 |
|   |   |    | 1  | 2 | 1 | n=2 |
|   |   | 1  | 3  | 3 | 1 | n=3 |
|   | 1 | 4  | 6  | 4 | 1 | n=4 |
| 1 | 5 | 10 | 10 | 5 | 1 | n=5 |

Obs

erve, that the coefficients of base  $n=2$  create the last column in the *lowpass* Pascal matrix of (8) with the exception of the elements in the even rows which have negative values. We have concluded that the *lowpass* Pascal matrix can be formed by taking into account the following rules (Biolkova and Biolek, 1999); (Pham and Psenicka, 1985).

- In the first row of the Pascal matrix all the elements must be equal to one.
- The elements of the last column can be computed using:

$$P_{i, i+1} = (-1)^{i-1} \frac{n!}{(n-i+1)!(i-1)!} \tag{12}$$

where

$$i=1, 2, \dots, n+1$$

The remaining elements  $P_{i,j}$  of the *lowpass* Pascal matrix can be determined using the following equation:

$$P_{i,j} = P_{i-1,j} + P_{i-1,j+1} + P_{i,j+1}$$

where

$$\begin{aligned} i &= 2, 3, 4, \dots, n, n+1 \\ j &= n, n-1, n-2, \dots, 2, 1 \end{aligned} \quad (13)$$

Without loss of generality, using letters of the alphabet in the order shown below we can identify the elements of the *lowpass* Pascal matrix for  $n=4$ :

$$\begin{bmatrix} a=1 & b=1 & c=1 & d=1 & e=1 \\ j & i & h & g & f=-4 \\ ? & ? & ? & ? & k=6 \\ ? & ? & ? & ? & l=-4 \\ ? & ? & ? & ? & p=1 \end{bmatrix} \quad (14)$$

where the elements denoted  $g, h, i$  and  $j$  can be obtained using the next set of equations:

$$\begin{aligned} g &= d + e + f = -2; & h &= c + d + g = 0 \\ i &= b + c + h = 2; & j &= a + b + i = 4 \end{aligned} \quad (15)$$

Then the *lowpass* Pascal matrix for the particular case of  $n=4$  is finally given by:

$$\bar{P}_{LP}^{(4)} = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 \\ 4 & 2 & 0 & -2 & -4 \\ 6 & 0 & -2 & 0 & 6 \\ 4 & -2 & 0 & 2 & -4 \\ 1 & -1 & 1 & -1 & 1 \end{bmatrix} \quad (16)$$

### Lowpass-to-highpass Transformation

In this second case, in order to transform the lowpass transfer function to the discrete

highpass transfer function  $H(z)$ , we substitute the variable  $s$  by  $1/s$  in (4). Thus,

$$s = k \frac{z+1}{z-1}$$

with

$$k = \tan \frac{\pi f_c}{f_s} \quad (17)$$

where  $f_c$  represents the cut-off frequency of the highpass and  $f_s$  the sampling frequency. Following the same process, substituting (17) into (1) and comparing the numerator with (3) for  $n=3$  and  $m=3$ , we can obtain:

$$\begin{aligned} &a_0 + a_1 z^{-1} + a_2 z^{-2} + a_3 z^{-3} = \\ &A_0 + A_1 k + A_2 k^2 + A_3 k^3 + \\ &+ z^{-1}(-3A_0 - A_1 k + A_2 k^2 + 3A_3 k^3) + \\ &+ z^{-2}(3A_0 - A_1 k - A_2 k^2 + 3A_3 k^3) + \\ &+ z^{-3}(-A_0 + A_1 k - A_2 k^2 + A_3 k^3) \end{aligned} \quad (18)$$

Again, equating the coefficients of the like powers in  $z$ , we obtain the following matrix equation

$$\begin{bmatrix} a_0 \\ a_1 \\ a_2 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 \\ -3 & -1 & 1 & 3 \\ 3 & -1 & -1 & 3 \\ -1 & 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} A_0 \\ A_1 k \\ A_2 k^2 \\ A_3 k^3 \end{bmatrix} \quad (19)$$

This equation can be written in the compact form

$$\bar{a} = \bar{P}_{HP}^{(3)} \times \bar{A} \quad (20)$$

where  $\bar{P}_{HP}^{(3)}$  is a variant of a Pascal matrix which corresponds to the highpass filter in which the first row elements are all equal to one, and the elements of the first column can

be obtained using (12). The remaining elements  $P_{i,j}$  can be determined using the following expression (Põeni, ka *et al.*, 2002):

$$P_{i,j} = P_{i,j-1} + P_{i-1,j-1} + P_{i-1,j}$$

Where  $i = 2, 3, \dots, n+1$  (21)

$$j = 2, 3, \dots, n+1$$

A similar development can be done for the denominator vector  $\bar{b}$ .

### Lowpass-to-bandpass Transformation

The latest case considered in this paper shows how to obtain a discrete bandpass filter (Konopacki, 2005) characterized by the discrete-time transfer function  $H(z)$

$$H(z) = \frac{a_0 + a_1 z^{-1} + a_2 z^{-2} + \dots + a_n z^{-n}}{b_0 + b_1 z^{-1} + b_2 z^{-2} + \dots + b_n z^{-n}} \quad (22)$$

which also has real coefficients  $a_i$  and  $b_i$ . As previously this transfer function can be obtained from the continuous one (1) by  $s$ - $z$  transformation. The bandpass filter can be seen as a superposition of a lowpass filter and a highpass filter (Rabiner and Gold, 1975). Thus, the  $s$ - $z$  transformation that applies is (Bose, 1985):

$$s = c \frac{z-1}{z+1} + k \frac{z+1}{z-1} \quad (23)$$

where  $c = \cot(\pi \frac{f_1}{f_s})$   $k = \tan(\pi \frac{f_{-1}}{f_s})$

$f_1$  and  $f_{-1}$  represent the upper and lower frequencies of the bandpass filter respectively, and  $f_s$  the sampling frequency.

In a similar manner from (22), we define the coefficient vectors  $\bar{a}$  and  $\bar{b}$ :

$$\begin{aligned} \bar{a}(a_0, a_1, a_2, \dots, a_n) \\ \bar{b}(b_0, b_1, b_2, \dots, b_n) \end{aligned} \quad (24)$$

In order to obtain the coefficients  $a_i$  and  $b_i$  ( $i = 0, 1, \dots, n$ ) knowing the continuous time representation vectors  $\bar{A}$  and  $\bar{B}$ , we must first substitute (23) into (1) then compare the numerator and denominator of the resulting transfer function with the corresponding ones in (22).

For example without loss of generalization we take  $m=1$  in (1), due to the high order terms appearing in the transformation (23), a  $n=2$  must taken in (22) resulting in:

$$H(z) = \frac{A(z)}{B(z)} = \frac{a_0 + a_1 z^{-1} + a_2 z^{-2}}{b_0 + b_1 z^{-1} + b_2 z^{-2}} =$$

$$\frac{A_0 + A_1 c + A_1 k + z^{-1} (2 A_1 k - 2 A_1 c) +}{B_0 + B_1 c + B_1 k + z^{-1} (2 B_1 k - 2 B_1 c) +} \quad (25)$$

$$\frac{+z^{-2} (-A_0 + A_1 c + A_1 k)}{+z^{-2} (-B_0 + B_1 c + B_1 k)}$$

and the following matrix equation:

$$\begin{bmatrix} a_0 \\ a_1 \\ a_2 \end{bmatrix} \begin{bmatrix} 1 & 1 & 1 \\ -2 & 0 & 2 \\ 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} A_1 c \\ A_0 \\ A_1 k \end{bmatrix} \quad (26)$$

A similar equation is obtained for the denominator vector  $\bar{b}$ . Both equations can be represented in the following compact form:

$$\bar{a} = \bar{P}_{BP}^n \times \bar{A}^m \quad (27)$$

$$\bar{b} = \bar{P}_{BP}^n \times \bar{B}^m$$

where  $\bar{P}_{BP}^n$  is the so called *bandpass* Pascal matrix. This matrix transforms the normalized lowpass to bandpass transfer function. We have named this matrix the bandpass

Pascal matrix (Psenicka and García-Ugalde, 2004) because the matrices of all orders have in the first column the coefficients of the base of a Pascal triangle (11) with the exception of elements in even rows, which have negative signs. In this example the vectors  $\overline{A}'''$  and  $\overline{B}'''$  are represented respectively by

$$\overline{A}''' = (A_1 c, A_0, A_1 k) \tag{28}$$

$$\overline{B}''' = (B_1 c, B_0, B_1 k)$$

In order to achieve an alternative representation of the original *bandpass* Pascal matrix, without lost of generality let us consider the case of order  $m=2$  and again because of the high order terms appearing in the transformation (23), a  $n=4$  must be taken. The matrix representation of  $\overline{a} = \overline{P}^n \times \overline{A}'''$  is given by

$$\begin{bmatrix} a_0 \\ a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ -4 & -2 & 0 & 2 & 4 & 0 \\ 6 & 0 & -2 & 0 & 6 & -2 \\ -4 & 2 & 0 & -2 & 4 & 0 \\ 1 & -1 & 1 & -1 & 1 & 1 \end{bmatrix} \times \begin{bmatrix} A_2 c^2 \\ A_1 c \\ A_0 \\ A_1 k \\ A_2 k^2 \\ 2 A_2 c k \end{bmatrix} \tag{29}$$

Note from this latest example that the matrix is rectangular and it will be the general case in a *lowpass-to-bandpass* transformation for values of  $m=2$  or higher. In order to use the same rules as in the previous section for the *lowpass-to-highpass* transformation (which always has a square matrix) we decompose this rectangular matrix into the concatenation of two matrices as shown in the following equation

$$\left[ \overline{P}^n \right] = \left[ \overline{S}_{BP}^n \left| \overline{R}_{BP}^n \right. \right] \tag{30}$$

In this equation the matrix  $\overline{S}_{BP}^n$  is square and its computation is exactly the same as that used in the *lowpass-to-highpass* transformation, which means: all the terms in the first column can be obtained using (12) and the remaining elements  $S_{ij}$  can be established using the following expression (Psenicka et al, 2002):

$$S_{ij} = S_{i,j-1} + S_{i-1,j-1} + S_{i-1,j}$$

Where  $i = 2, 3, \dots, n+1$  (31)

$$j = 2, 3, \dots, n+1$$

On the other hand the matrix  $\overline{R}_{BP}^n$  in (30) is rectangular with  $n+1$  rows. A priori the number of columns has to be computed by counting the number of elements different to 1 included in the upper triangle from base  $m$  of the Pascal triangle (11). To illustrate these values we summarize in table 1 the number of columns *col* of matrix  $\overline{R}_{BP}^n$  for different  $m$  and  $n$  parameter values.

Table 1. Number of columns *col* in the matrix  $\overline{R}_{BP}^n$

| $m$ | $n$ | <i>col</i> |
|-----|-----|------------|
| 2   | 4   | 1          |
| 3   | 6   | 3          |
| 4   | 8   | 6          |

Once the elements of matrix  $\overline{S}_{BP}^n$  are known the columns of  $\overline{R}_{BP}^n$  can be derived directly. Let us consider the case  $m=2$ , the lonely column of  $\overline{R}_{BP}^n$  is equal to the central column of  $\overline{S}_{BP}^n$  (Psenicka and García-Ugalde, 2004). In this paper we call this column *the pivot* because for  $m=2$  there is only one element different to 1 in the upper triangle from base  $m$  in the Pascal triangle and its position corresponds to a central position in the triangle. For  $m=3$ , as shown in table 1,

there are three columns in  $\bar{R}_{BP}^n$ , one is also the pivot because again it is equal to the central column of  $\bar{S}_{BP}^n$  and the two others are the columns on the right of the pivot and on the left of it. Also the reason is because for  $m=3$  there are three elements different to one in the upper triangle from base  $m$  and their positions correspond to a central position in the triangle plus its nearest neighbors (right and left). To illustrate the previous structure we show the resulting  $\bar{P}_{BP}^n$  matrix for vector  $\bar{a}$  and parameters  $m=3, n=6$ .

$$\begin{bmatrix} a_0 \\ a_1 \\ a_2 \\ a_3 \\ a_4 \\ a_5 \\ a_6 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 & 1 \\ -6 & -4 & -2 & 0 & 2 & 4 & 6 & 0 & 2 & -2 \\ 15 & 5 & -1 & -3 & -1 & 5 & 15 & -3 & -1 & -1 \\ -20 & 0 & 4 & 0 & -4 & 0 & 20 & 0 & -4 & 4 \\ 15 & -5 & -1 & 3 & -1 & -5 & 15 & 3 & -1 & -1 \\ -6 & 4 & -2 & 0 & 2 & -4 & 6 & 0 & 2 & -2 \\ 1 & -1 & 1 & -1 & 1 & -1 & 1 & -1 & 1 & 1 \end{bmatrix}$$

$$\times \begin{bmatrix} A_3 c^3 \\ A_2 c^2 \\ A_1 c \\ A_0 \\ A_1 k \\ A_2 k^2 \\ A_3 k^3 \\ 2 A_2 c k \\ 3 A_3 c k^2 \\ 3 A_3 c^2 k \end{bmatrix} \quad (32)$$

A similar expression can be obtained for vector  $\bar{b}$ .

### Inverse Transformation from H(z) to H(s)

The inverse Pascal matrix is defined by the following equation (Klein, 1976):

$$\bar{P}_n^{-1} = 2^{-n} \times \bar{P}_n \quad (33)$$

In all cases using the inverse Pascal matrix the continuous-time transfer function  $H(s)$  can be obtained from the transfer matrix of the discrete-time structure  $H(z)$ . The advantage of using this equation is that to compute the inverse Pascal matrix the determinant of the system is not necessary.

For example consider the lowpass case, let  $H(z)$  be the transfer function of the discrete structure that works at the corner frequency  $f_1 = 3400$  [Hz] and sampling frequency  $f_s = 16000$  [Hz].

$$H(z) = \frac{0.227 + 0.454z^{-1} + 0.227z^{-2}}{1 - 0.276z^{-1} + 0.185z^{-2}} \quad (34)$$

First it is necessary to calculate the constant  $c$  of the bilinear transform (1):

$$c = \cot\left(\frac{\pi 3400}{16000}\right) = 126849 \quad (35)$$

Then the transfer function coefficients of the analog circuit will be calculated as follows:

$$\begin{bmatrix} A_0 \\ A_1 c \\ A_2 c^2 \end{bmatrix} = \frac{1}{4} \begin{bmatrix} 1 & 1 & 1 \\ 2 & 0 & -2 \\ 1 & -1 & 1 \end{bmatrix} \begin{bmatrix} 0.227 \\ 0.454 \\ 0.227 \end{bmatrix} = \begin{bmatrix} 0.227 \\ 0.0 \\ 0.0 \end{bmatrix} \quad (36)$$

$$\begin{bmatrix} B_0 \\ B_1 c \\ B_2 c^2 \end{bmatrix} = \frac{1}{4} \begin{bmatrix} 1 & 1 & 1 \\ 2 & 0 & -2 \\ 1 & -1 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ -0.276 \\ 0.185 \end{bmatrix} = \begin{bmatrix} 0.227 \\ 0.407 \\ 0.365 \end{bmatrix} \quad (37)$$

and

$$A_0 = 0.227 \quad A_1 = 0.0 \quad A_2 = 0.0$$

$$B_0 = 0.227 \quad B_1 = 0.321 \quad B_2 = 0.227$$

The transfer function of the corresponding analog filter is the Butterworth transfer function of the second order:

$$H(s) = \frac{0.227}{0.227s^2 + 0.321s + 0.227} = \frac{1}{s^2 + 1.4142s + 1}$$

### Numerical Examples

In these examples we shall transform a lowpass transfer function  $H(s)$  to lowpass and highpass transfer functions  $H(z)$  using the features specified by:

$$c = k = 1, \quad f_s = 8000[\text{Hz}], \quad (38)$$

$$H(s) = \frac{s^2 + 5.153}{0.929s^3 + 2.781s^2 + 4.344s + 5.153}$$

*Transformation LP-to-LP from s to the z domain*

The transfer function coefficients  $a_i, b_i$ , for  $i=0,1,2,3$  can then be obtained using the equations:

$$\begin{bmatrix} a_0 \\ a_1 \\ a_2 \\ a_3 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 \\ 3 & 1 & -1 & -3 \\ 3 & -1 & -1 & 3 \\ 1 & -1 & 1 & -1 \end{bmatrix} \times \begin{bmatrix} A_0 \\ A_1 c \\ A_2 c^2 \\ A_3 c^3 \end{bmatrix} = \quad (39)$$

$$= \begin{bmatrix} 1 & 1 & 1 & 1 \\ 3 & 1 & -1 & -3 \\ 3 & -1 & -1 & 3 \\ 1 & -1 & 1 & -1 \end{bmatrix} \times \begin{bmatrix} 5.153 \\ 0.0 \\ 1.0 \\ 0.0 \end{bmatrix}$$

$$\begin{bmatrix} b_0 \\ b_1 \\ b_2 \\ b_3 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 \\ 3 & 1 & -1 & -3 \\ 3 & -1 & -1 & 3 \\ 1 & -1 & 1 & -1 \end{bmatrix} \times \begin{bmatrix} B_0 \\ B_1 c \\ B_2 c^2 \\ B_3 c^3 \end{bmatrix} = \quad (40)$$

$$= \begin{bmatrix} 1 & 1 & 1 & 1 \\ 3 & 1 & -1 & -3 \\ 3 & -1 & -1 & 3 \\ 1 & -1 & 1 & -1 \end{bmatrix} \times \begin{bmatrix} 5.153 \\ 4.344 \\ 2.781 \\ 0.929 \end{bmatrix}$$

given

$$a_0 = 61.53, a_1 = 14.459, a_2 = 14.459, a_3 = 6.153$$

$$b_0 = 13.207, b_1 = 14.235, b_2 = 11.121, b_3 = 2.661$$

The transfer function  $H(z)$  takes the form

$$H(z) = \frac{0.4658 + 1.0948z^{-1} + 1.0948z^{-2} + 0.4658z^{-3}}{1 + 1.0778z^{-1} + 0.842z^{-2} + 0.2015z^{-3}} \quad (41)$$

For this equation the corresponding magnitude and phase frequency responses of the digital lowpass filter are shown in Figure 1.



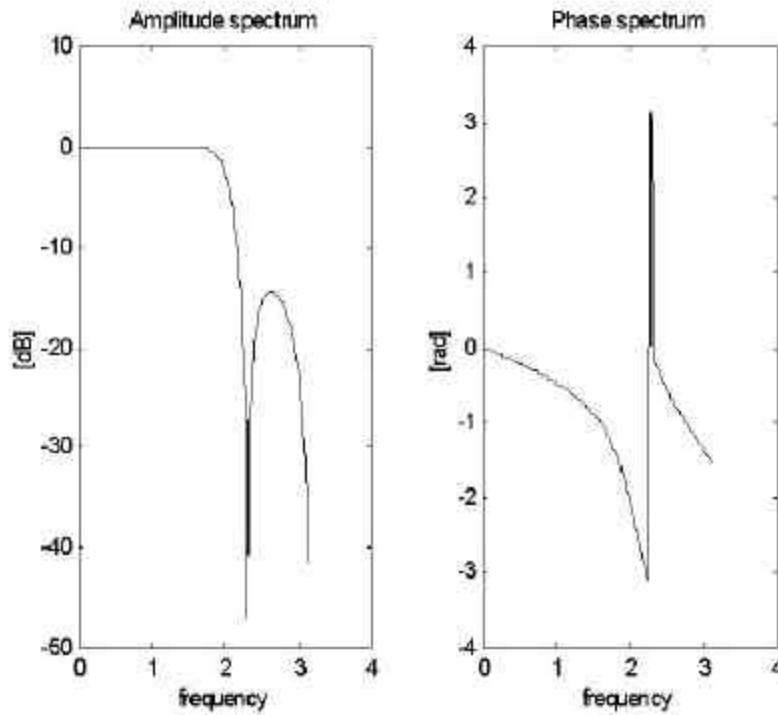


Figure 1. Magnitude and phase frequency responses of the lowpass filter

Transformation LP-to-HP from  $s$  to the  $z$  domain

Using the Pascal matrix  $\bar{P}_{HP}^{(3)}$  we can transform the lowpass transfer function (38) to the highpass transfer function  $H(z)$  using the following equations:

$$\begin{bmatrix} b_0 \\ b_1 \\ b_2 \\ b_3 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 \\ -3 & -1 & 1 & 3 \\ 3 & -1 & -1 & 3 \\ -1 & 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} B_0 \\ B_1 k \\ B_2 k^2 \\ B_3 k^3 \end{bmatrix}$$

(43)

$$\begin{bmatrix} a_0 \\ a_1 \\ a_2 \\ a_3 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 \\ -3 & -1 & 1 & 3 \\ 3 & -1 & -1 & 3 \\ -1 & 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} A_0 \\ A_1 k \\ A_2 k^2 \\ A_3 k^3 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 \\ -3 & -1 & 1 & 3 \\ 3 & -1 & -1 & 3 \\ -1 & 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} 5.153 \\ 4.344 \\ 2.781 \\ 0.929 \end{bmatrix}$$

(42)

The coefficients of the highpass transfer function are:

$$a_0 = 6153, \quad a_1 = -14.459$$

$$a_2 = 14.459, \quad a_3 = 6153$$

$$b_0 = 13.207, \quad b_1 = -14.235$$

$$= \begin{bmatrix} 1 & 1 & 1 & 1 \\ -3 & -1 & 1 & 3 \\ 3 & -1 & -1 & 3 \\ -1 & 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} 5.153 \\ 0.0 \\ 1.0 \\ 0.0 \end{bmatrix}$$

$$b_2 = 11.121, \quad b_3 = -2.661$$

and the highpass transfer function is given by (44). The magnitude and phase frequency responses of the digital highpass filter are shown in Figure 2.

$$H(z) = \tag{44}$$

$$= \frac{0.4658 - 10.948z^{-1} + 10.948z^{-2} - 0.4658z^{-3}}{1 - 1.0778z^{-1} + 0.842z^{-2} - 0.2015z^{-3}}$$

*Transformation LP-to-BP from s to the z domain*

In this example we transform a Butterworth lowpass transfer function  $H(s)$  to a bandpass transfer function  $H(z)$  using the features specified by:

$$f_1 = 3000 \text{ [Hz]}, \quad f_{-1} = 1000 \text{ [Hz]}$$

$$f_s = 8000 \text{ [Hz]} \tag{45}$$

$$H(s) = \frac{1}{s^2 + \sqrt{2}s + 1}$$

In order to transform the lowpass analog function (45) into the digital bandpass function, we must first determine the transfer function coefficients  $a_i, b_i$  for  $i=0,1,\dots,4$  which can be obtained using the matrix equations for current values:

$$c = \cot\left(\frac{\pi 3000}{8000}\right) = 0.4142$$

$$k = \tan\left(\frac{\pi 1000}{8000}\right) = 0.4142$$

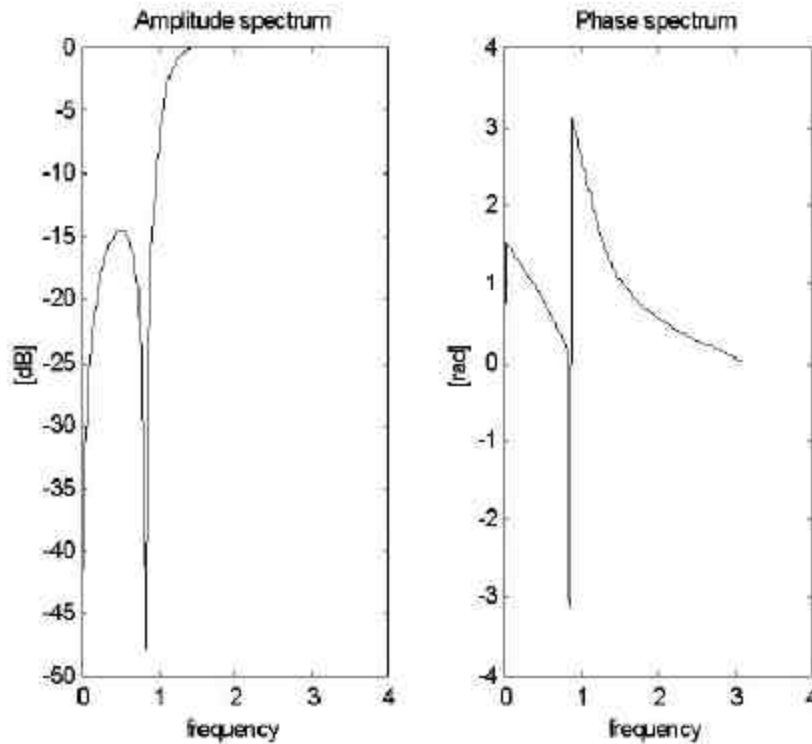


Figure 2. Magnitude and phase frequency responses of the highpass filter

$$\begin{bmatrix} a_0 \\ a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ -4 & -2 & 0 & 2 & 4 & 0 \\ 6 & 0 & -2 & 0 & 6 & -2 \\ -4 & 2 & 0 & -2 & 4 & 0 \\ 1 & -1 & 1 & -1 & 1 & 1 \end{bmatrix} \times \begin{bmatrix} A_2 c^2 \\ A_1 c \\ A_0 \\ A_1 k \\ A_2 k^2 \\ 2 A_2 ck \end{bmatrix} = \quad (46)$$

$$= \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ -4 & -2 & 0 & 2 & 4 & 0 \\ 6 & 0 & -2 & 0 & 6 & -2 \\ -4 & 2 & 0 & -2 & 4 & 0 \\ 1 & -1 & 1 & -1 & 1 & 1 \end{bmatrix} \times \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ -2 \\ 0 \\ 1 \end{bmatrix}$$

$$\begin{bmatrix} b_0 \\ b_1 \\ b_2 \\ b_3 \\ b_4 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ -4 & -2 & 0 & 2 & 4 & 0 \\ 6 & 0 & -2 & 0 & 6 & -2 \\ -4 & 2 & 0 & -2 & 4 & 0 \\ 1 & -1 & 1 & -1 & 1 & 1 \end{bmatrix} \times \begin{bmatrix} B_2 c^2 \\ B_1 c \\ B_0 \\ B_1 k \\ B_2 k^2 \\ 2 B_2 ck \end{bmatrix} = \quad (47)$$

$$= \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ -4 & -2 & 0 & 2 & 4 & 0 \\ 6 & 0 & -2 & 0 & 6 & -2 \\ -4 & 2 & 0 & -2 & 4 & 0 \\ 1 & -1 & 1 & -1 & 1 & 1 \end{bmatrix} \times \begin{bmatrix} 0.1716 \\ 0.5858 \\ 1 \\ 0.5858 \\ 0.1716 \\ 0.3431 \end{bmatrix} = \begin{bmatrix} 2.8579 \\ 0 \\ -0.627 \\ 0 \\ 0.5147 \end{bmatrix}$$

The transfer function of the bandpass filter is given by

$$H(z) = \frac{0.3499 - 0.6998z^{-2} + 0.3499z^{-4}}{1 - 0.2194z^{-2} + 0.1801z^{-4}} \quad (48)$$

Finally, a more complicated example is presented, in which the lowpass transfer function  $H(s)$  contains two transfer functions  $H_1(s)$  and  $H_2(s)$  and is transformed into the whole system bandpass transfer function  $H(z)$  for  $f_i = 3000[Hz]$ ,  $f_{-1} = 1000[Hz]$ ,  $f_s = 8000[Hz]$

$$H(s) = H_1(s) \times H_2(s) = \quad (49)$$

$$\frac{0.123}{s + 0.3497} \times \frac{s^2 + 0.2897}{s^2 + 0.0492s + 0.2492}$$

In order to transform the lowpass analog function (49) into the digital bandpass function, we proceed the  $s$ - $z$  transformation for each of these two transfer functions, we must first establish the coefficients  $a_i, b_i$ , for  $i=0,1,2$  for the first function  $H_1(z)$  and then the coefficients  $a_i, b_i$ , for  $i=0,1,2,\dots,4$  for the second one  $H_2(z)$ . This computation can be obtained using the matrix equations previously defined for current values:

$$c = \cot\left(\frac{\pi 3000}{8000}\right) = 0.4142$$

$$k = \tan\left(\frac{\pi 1000}{8000}\right) = 0.4142$$

$$\begin{bmatrix} a_0 \\ a_1 \\ a_2 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ -2 & 0 & 2 \\ 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} A_1 c \\ A_0 \\ A_1 k \end{bmatrix} = \quad (50)$$

$$= \begin{bmatrix} 1 & 1 & 1 \\ -2 & 0 & 2 \\ 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} 0 \\ 0.123 \\ 0 \end{bmatrix} = \begin{bmatrix} 0.123 \\ 0 \\ -0.123 \end{bmatrix}$$

$$\begin{bmatrix} b_0 \\ b_1 \\ b_2 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ -2 & 0 & 2 \\ 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} B_1 c \\ B_0 \\ B_1 k \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ -2 & 0 & 2 \\ 1 & -1 & 1 \end{bmatrix} \times \begin{bmatrix} 0.4142 \\ 0.3497 \\ 0.4142 \end{bmatrix} = \begin{bmatrix} 1.1781 \\ 0 \\ 0.4787 \end{bmatrix} \quad (51)$$

$$\begin{bmatrix} a_0 \\ a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ -4 & -2 & 0 & 2 & 4 & 0 \\ 6 & 0 & -2 & 0 & 6 & -2 \\ -4 & 2 & 0 & -2 & 4 & 0 \\ 1 & -1 & 1 & -1 & 1 & 1 \end{bmatrix} \times \begin{bmatrix} A_2 c^2 \\ A_1 c \\ A_0 \\ A_1 k \\ A_2 k^2 \\ 2 A_2 ck \end{bmatrix} =$$

$$= \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ -4 & -2 & 0 & 2 & 4 & 0 \\ 6 & 0 & -2 & 0 & 6 & -2 \\ -4 & 2 & 0 & -2 & 4 & 0 \\ 1 & -1 & 1 & -1 & 1 & 1 \end{bmatrix} \times \begin{bmatrix} 0.1716 \\ 0.0204 \\ 0.2492 \\ 0.0204 \\ 0.1716 \\ 0.3431 \end{bmatrix} = \begin{bmatrix} 0.9763 \\ 0 \\ 0.8746 \\ 0 \\ 0.8946 \end{bmatrix} \quad (53)$$

The whole system transfer function in z of the bandpass filter is given in (54) and the corresponding magnitude and phase frequency responses are shown in Figure 3.

$$= \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ -4 & -2 & 0 & 2 & 4 & 0 \\ 6 & 0 & -2 & 0 & 6 & -2 \\ -4 & 2 & 0 & -2 & 4 & 0 \\ 1 & -1 & 1 & -1 & 1 & 1 \end{bmatrix} \times \begin{bmatrix} 0.1716 \\ 0 \\ 0.2897 \\ 0 \\ 0.1716 \\ 0.3431 \end{bmatrix} =$$

$$H(z) = H_1(z) \times H_2(z) = \frac{0.123 - 0.123z^{-2}}{1.1781 + 0.4787z^{-2}} \times \frac{0.976 + 0.7936z^{-2} + 0.976z^{-4}}{0.9763 + 0.8746z^{-2} + 0.8946z^{-4}} \quad (54)$$

$$= \begin{bmatrix} 0.976 \\ 0 \\ 0.7936 \\ 0 \\ 0.976 \end{bmatrix} \quad (52)$$

$$\begin{bmatrix} b_0 \\ b_1 \\ b_2 \\ b_3 \\ b_4 \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ -4 & -2 & 0 & 2 & 4 & 0 \\ 6 & 0 & -2 & 0 & 6 & -2 \\ -4 & 2 & 0 & -2 & 4 & 0 \\ 1 & -1 & 1 & -1 & 1 & 1 \end{bmatrix} \times \begin{bmatrix} B_2 c^2 \\ B_1 c \\ B_0 \\ B_1 k \\ B_2 k^2 \\ 2 B_2 ck \end{bmatrix} =$$

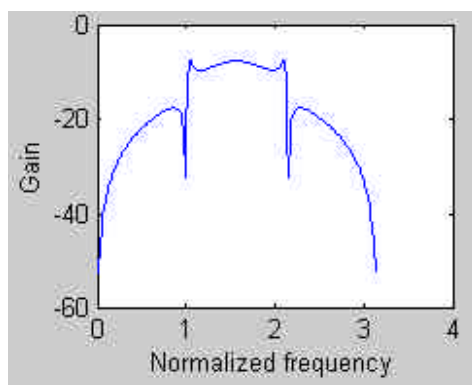


Figure 3. Magnitude and phase frequency responses of the Caer bandpass filter.

## Conclusions

The Pascal matrix is very useful in the context of the design of digital filters. Transformations can easily be done from the analog prototype lowpass transfer function  $H(s)$  to the discrete transfer function  $H(z)$  to obtain one of the main three types of digital filters: lowpass, highpass and bandpass. The inverse transformation from discrete to analog is very easy to achieve as well because we do not need to compute the determinant of the system. In this paper we have summarized all types of direct transformations and illustrate their use with several numerical examples. An alternative representation of the original bandpass Pascal matrix has been presented for the systematic computation of the bandpass Pascal matrix.

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## References

- Antoniou A. (1993). *Digital Filters: Analysis, Design, and Applications*. McGraw-Hill, New York, USA.
- Biolkova V. and Biolek D. (1999). Generalized Pascal Matrix of First Order  $s$ - $z$ . Transforms. *ICECS, Pafos, Cyprus*, Vol. 2, pp. 929-931, September.
- Bose N.K. (1985). *Digital Filters Theory and Applications*. Elsevier Science Publishing Co., Inc., Amsterdam, The Netherlands.
- Klein W. (1976). *Finite Systemtheorie*. B.G. Teubner Studienbücher, Stuttgart.
- Konopacki J. (2005). The frequency Transformation by Matrix Operation and its Application in iir Filters Design. *IEEE Signal Processing Letters*, Vol. 12, No. 1, pp. 5-8, January.
- Parks T.W. and Burrus C. (1987). *Digital Filter Design*. John Wiley and Sons, Inc., New York, USA.
- Pham Khac di and Põeni, ka B. (1985). Transfer Function Computation Using Pascal Matrix. *Electronic Horizon-Praha*, Vol 46-7, pp. 348-350.
- Põeni, ka B. and García-Ugalde F. (2004). Z-transform from Lowpass to Bandpass by Pascal Matrix. *IEEE Signal Processing Letters*, Vol. 11, No. 2, pp. 282-284, February.
- Põeni, ka B., García-Ugalde F. and Herrera-Camacho A. (2002). Z-transformation from Lowpass to Lowpass and Highpass Transfer Function. *IEEE Signal*

*Processing Letters*, Vol. 9, No. 11, pp. 368-370, November.

Rabiner R. and Gold B. (1975). *Theory and Applications of Digital Signal Processing*. Prentice-Hall, New Jersey, USA.

### **Suggesting Biography**

Bellanger M. (2000). *Digital Processing of Signals, Theory and Practice*. John Willey and Sons, Inc., Chichester, UK.

Manolakis D.G. and Proakis J.G. (1996). *Digital Signal Processing: Principles,*

*Algorithms, and Applications*. Prentice-Hall, New Jersey, USA.

Mitra S.K. and Kaiser J.F. (1993). *Handbook of Digital Signal Processing*. John Willey and Sons, Inc., New York, USA.

Oppenheim A.V. and Schaffer R.W. (1975). *Digital Signal Processing*. Prentice-Hall, New Jersey, USA.

Porat B. (2000). *A Course in Digital Signal Processing*. John Willey and Sons, Inc., New York, USA.

Rorabaugh C.B. (1993). *Digital Filter Designer's Handbook*. McGraw-Hill, New York, USA.

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